

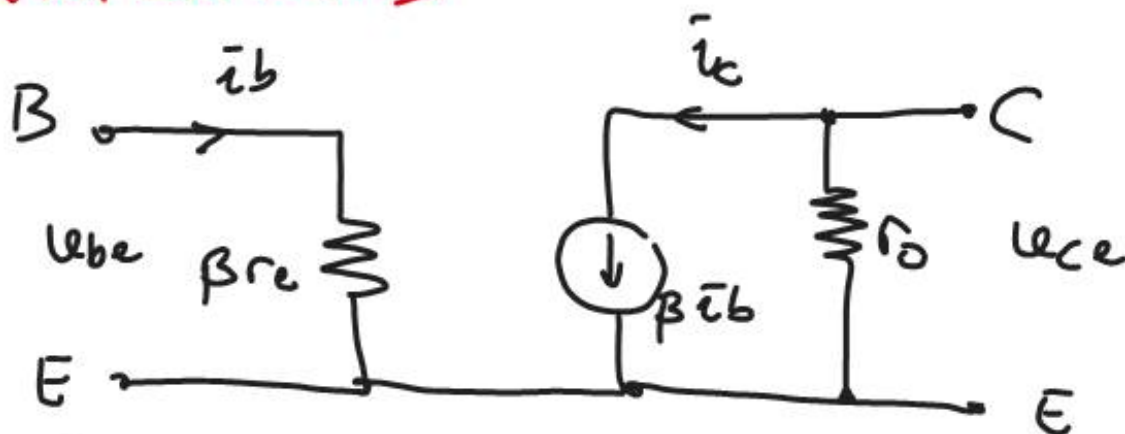
ECE 246

12.05.2012

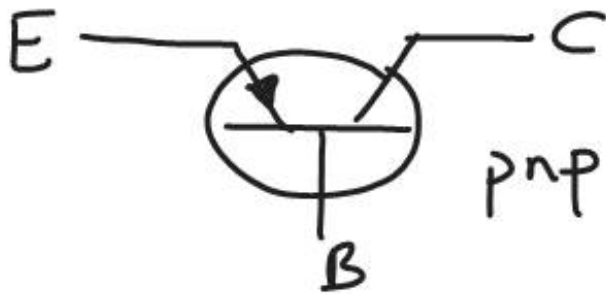
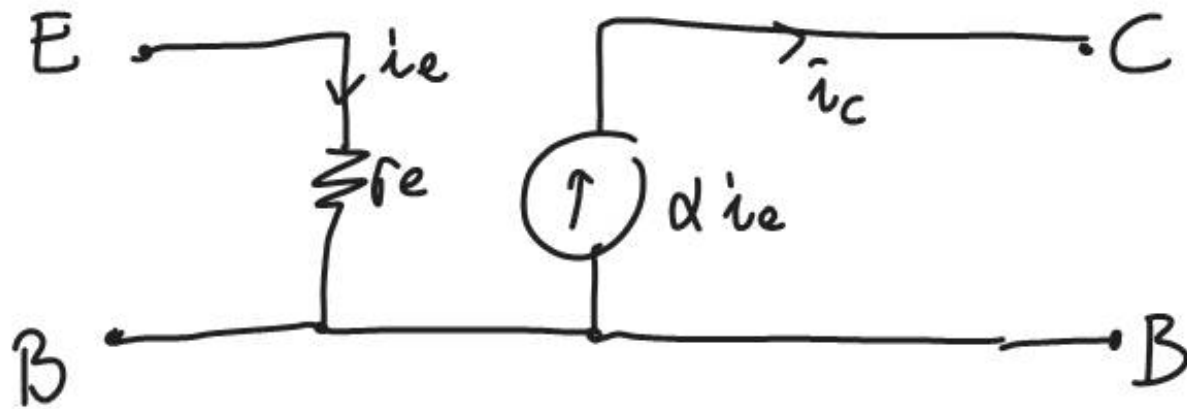
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BIPOLAR JUNCTION TRANSISTOR (BJT)

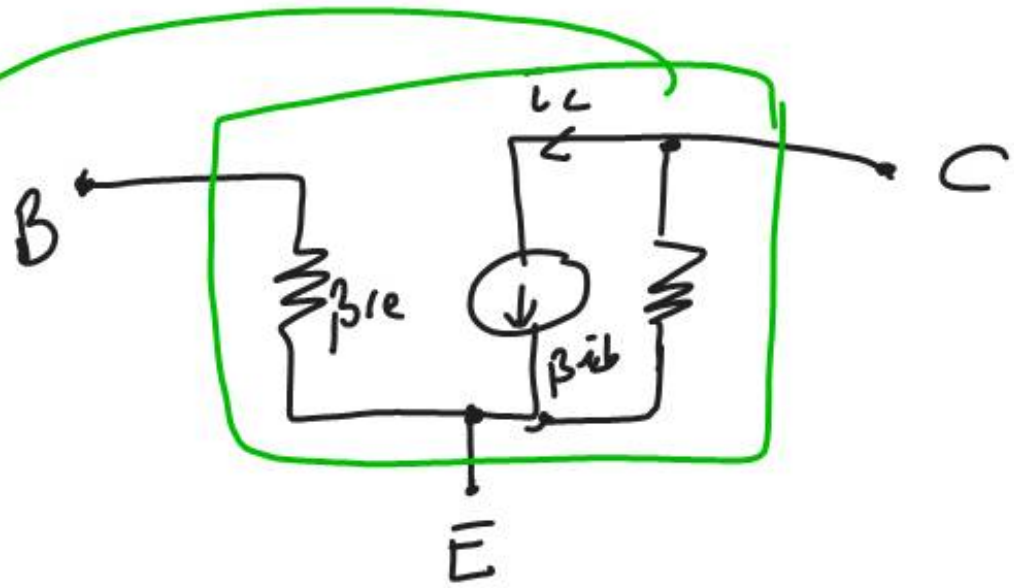
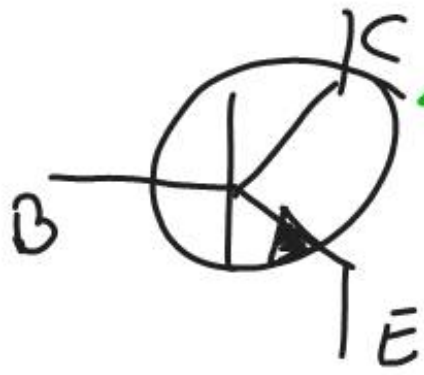
AMPLIFIERS



Common Emitter (CE) (we use the same BJT equivalent circuit for ac signals (small signals) for CC configuration as well)

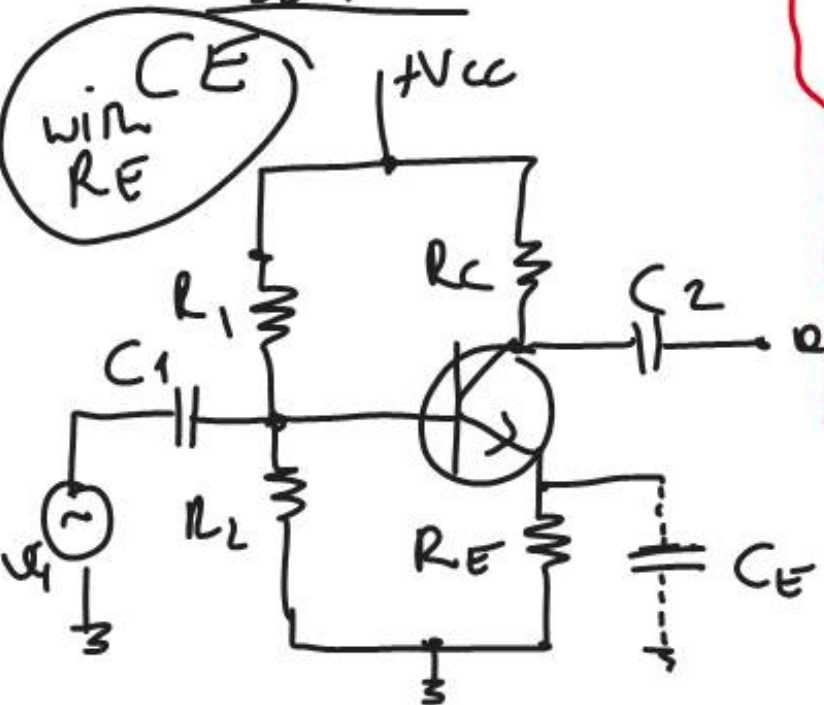


Common base
(CB)
equivalent



REMINDER

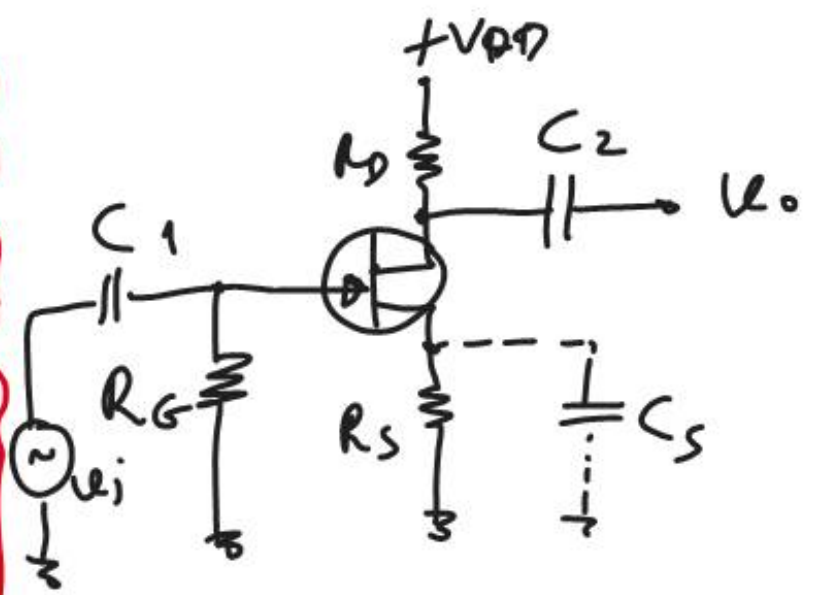
BJT



$$A_v = \frac{v_o}{v_i} = - \frac{R_C}{r_e} \text{ with } C_E$$

$$A_v \text{ or } = - \frac{R_C}{r_e + R_E} \text{ without } C_E$$

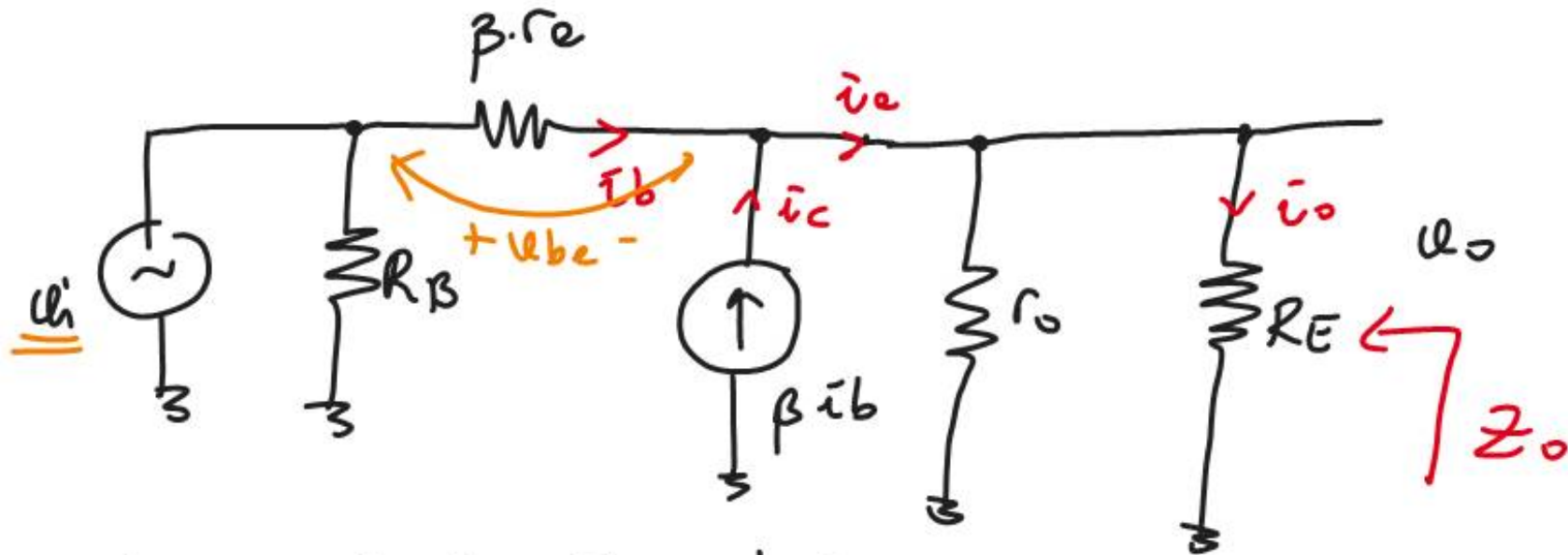
FET CS



$$A_v = -g_m R_D \text{ with } C_S$$

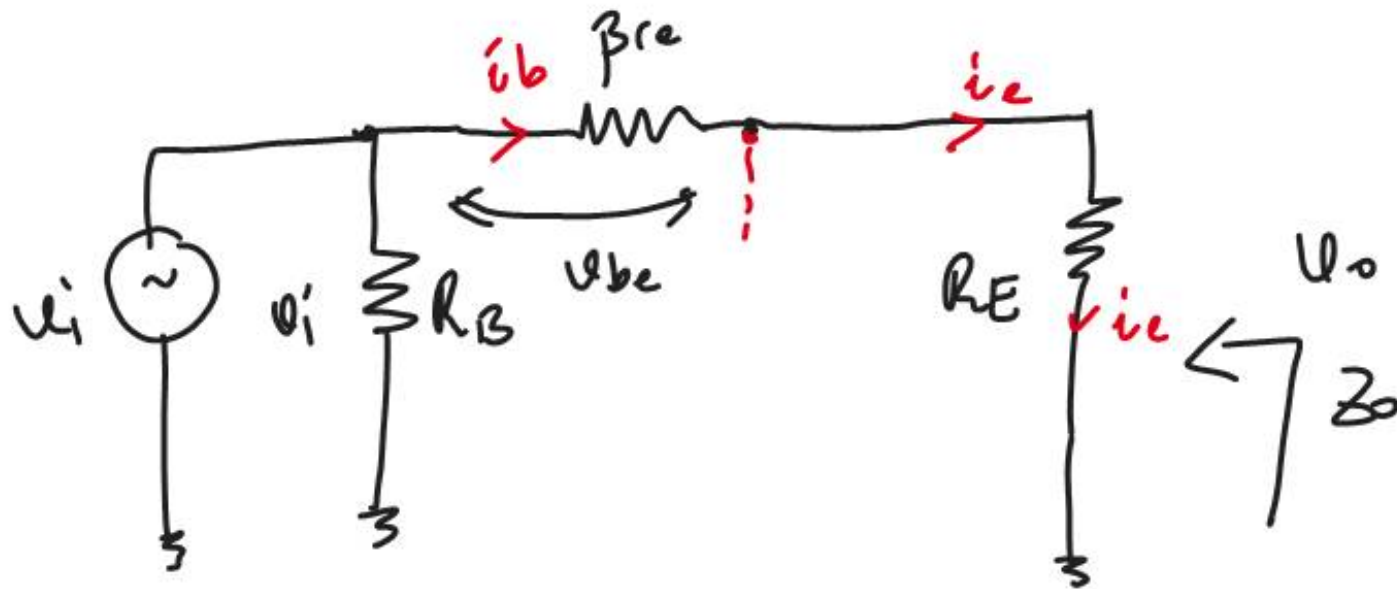
$$A_v = \frac{-g_m R_D}{1 + g_m R_S} \text{ without } C_S$$

Calculating Z_o in CC (Emitter Follower)

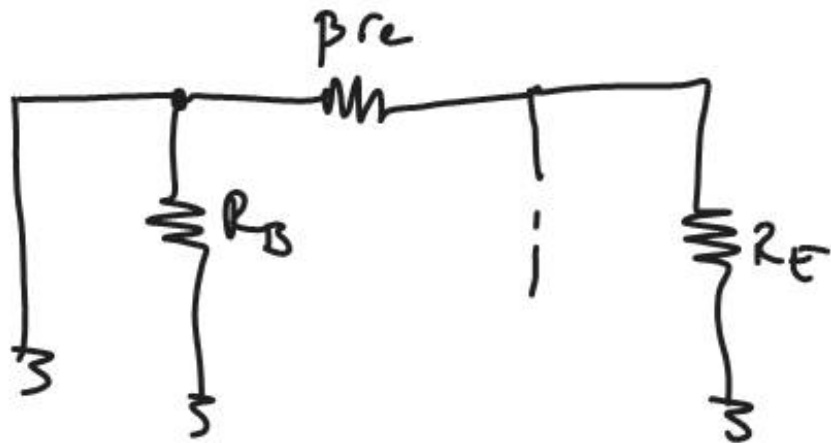


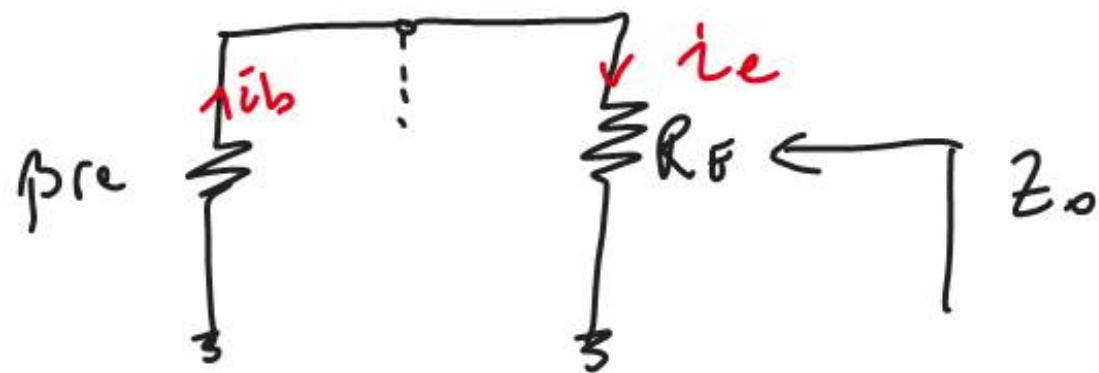
If we neglect r_o and the equivalent resistance of the current source in comparison with R_E as parallel:

$$Z_{\text{current source}} \parallel r_o \parallel R_E \approx R_E$$

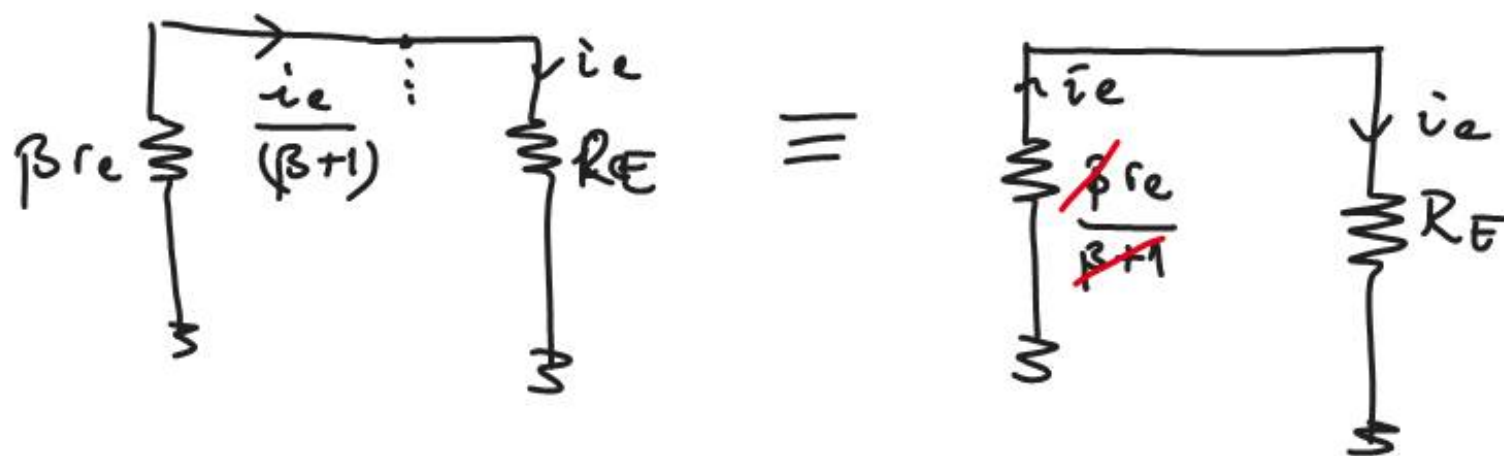


Short circuit input power supply when calculating Z_o (by definition)





We equalize the current in the circuit:





Calculation of A_{ve}

$$\begin{aligned}
 u_i &= u_{be} + u_o \\
 &= \bar{i}_b \cdot \beta \cdot r_e + \bar{i}_o \cdot R_E
 \end{aligned}$$

$$u_i \approx \bar{i}_b \cdot \beta \cdot r_e + \bar{i}_e \cdot R_E$$

$$u_i = \beta \cdot \bar{i}_b \cdot r_e + (\beta + 1) \bar{i}_b \cdot R_E \quad \beta \approx \beta + 1$$

$$u_i = \beta \bar{i}_b (r_e + R_E) \Rightarrow \bar{i}_b = \frac{u_i}{(\beta + 1)(r_e + R_E)}$$

$$u_o \approx \bar{i}_e \cdot R_E$$

$$= \beta \cdot \bar{i}_b \cdot R_E$$

$$u_o = \beta \left(\frac{u_i}{(\beta + 1)(r_e + R_E)} \right) \cdot R_E$$

$$\bar{i}_o \approx \bar{i}_e$$

$$\frac{u_o}{u_i} = A_{ve} = \frac{R_E}{r_e + R_E}$$

$$A_v = \frac{R_E}{r_e + R_E}$$

Voltage Gain of Emitter Follower Circuit

- $A_v < 1$

- output voltage is in the same phase ($\theta = 0^\circ$) with input voltage

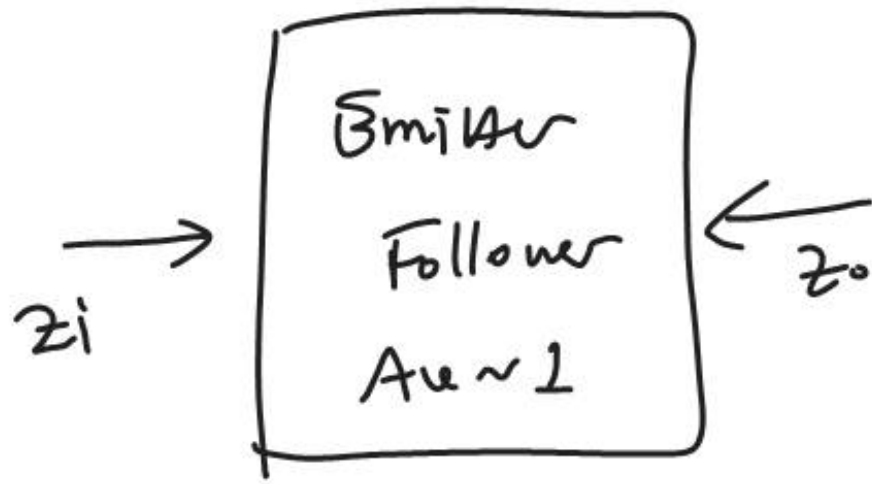
$$Z_i \cong R_B \parallel [\beta (r_e + R_E)]$$

very high input impedance

$$Z_o \cong r_e \parallel R_E \approx r_e$$

very low output impedance

Emitter follower circuit can be used as an
IMPEDANCE MATCHING CIRCUIT



$$z_i \approx R_B \parallel \beta (r_e + R_E)$$

$$z_o \approx r_e$$