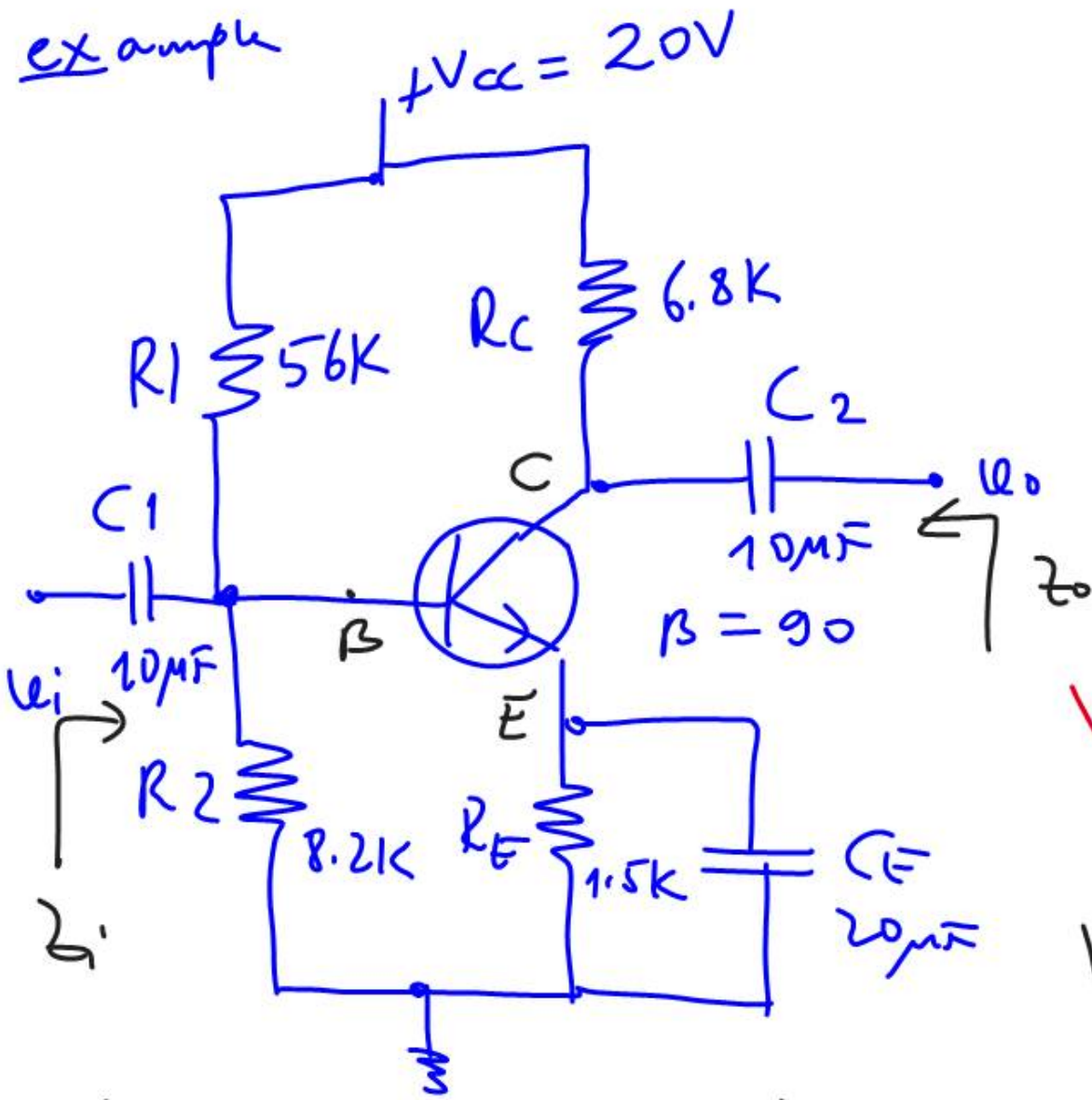
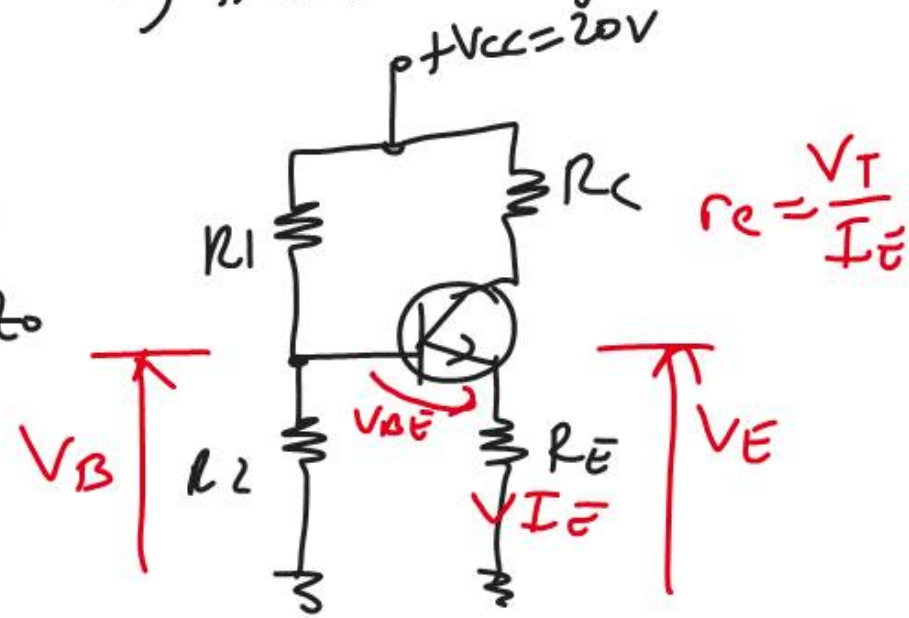


example

17.05.2011
 ©



a) DC Analysis



A_u, Z_i, Z_o
 A_i

$$V_E = V_O - V_{BE}$$

$$V_E = 2.6 - 0.7$$

$$\underline{V_E = 1.9V}$$

$$V_B = \frac{V_{CC} \cdot R_2}{R_1 + R_2}$$

$$V_B = \frac{20}{56.2} \times 8.2 \times 10^3$$

$$\leftarrow V_B = 2.55V \approx 2.6V$$

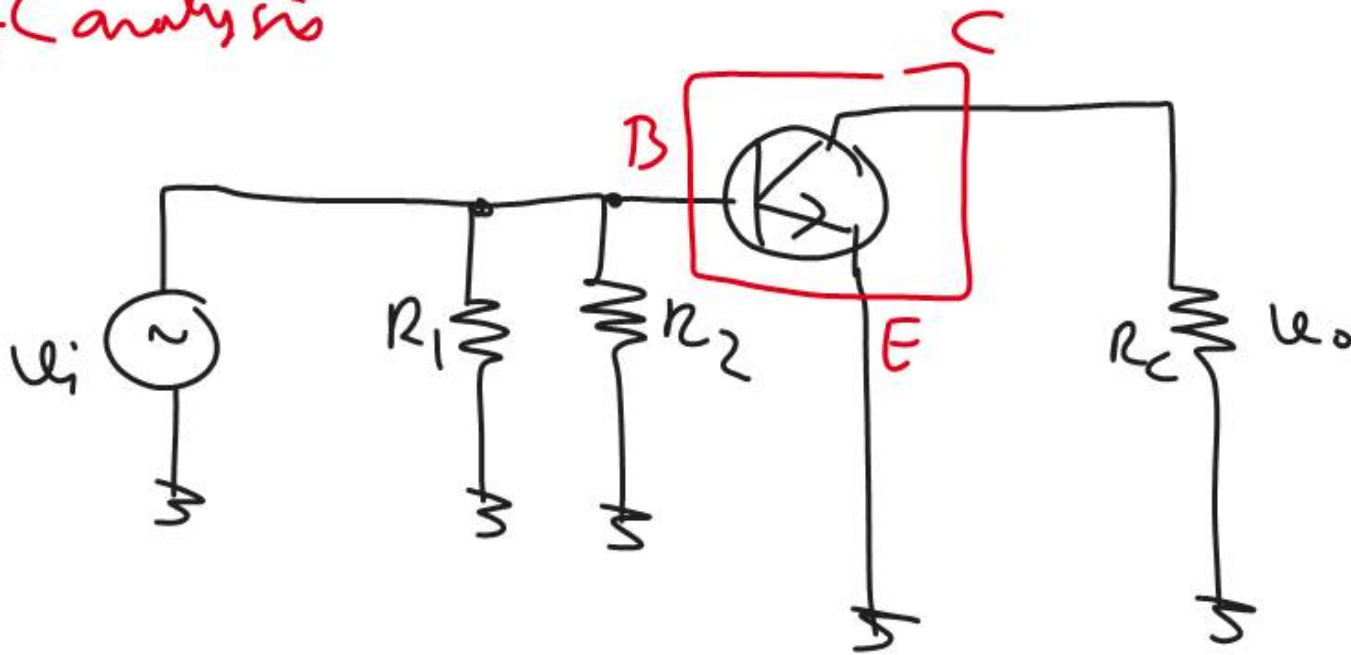
$$I_E = \frac{V_E}{R_E}$$

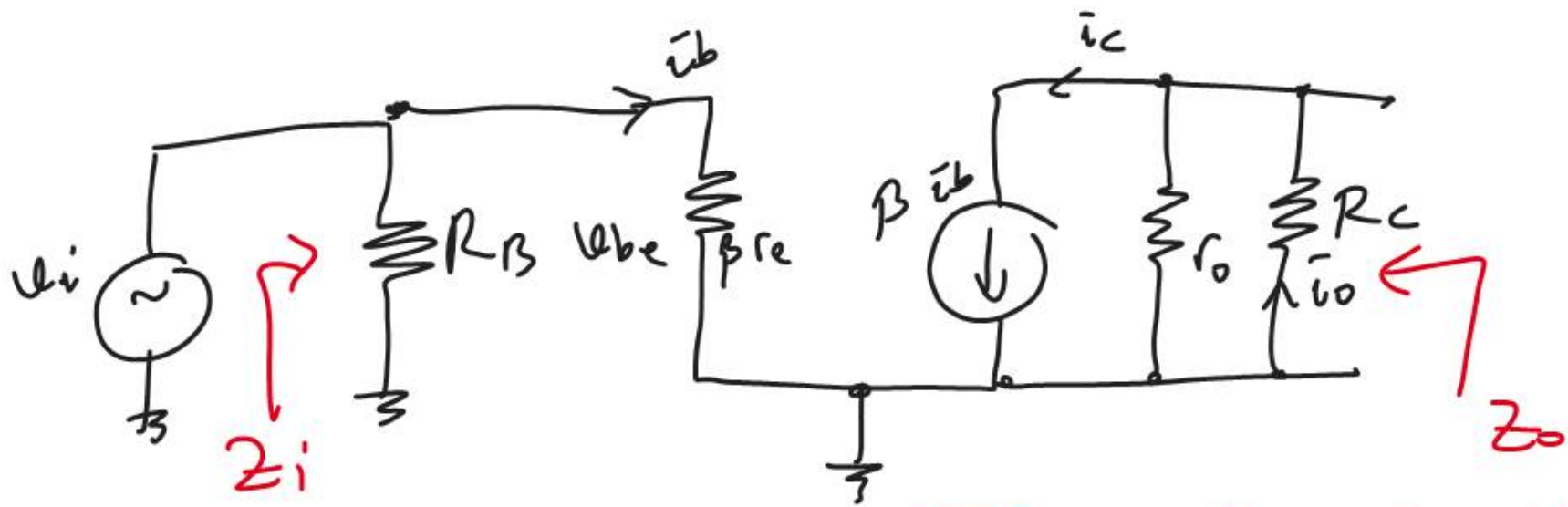
$$I_E = \frac{1.9}{1.5 \times 10^3}$$

$$\underline{I_E = 1.27 \text{ mA}}$$

$$r_e = \frac{26 \text{ mV}}{1.27 \text{ mA}} = \frac{26 \times 10^{-3}}{1.27 \times 10^{-3}} \approx 21 \Omega.$$

AC analysis





$$R_B = R_1 // R_2$$

$$Z_i = R_B // \beta r_e$$

$$A_u = \frac{u_o}{u_i}$$

$$u_i = u_{be}$$

$$i_b = \frac{u_{be}}{\beta r_e}$$

$$u_o = -i_o \cdot R_C$$

$$\text{if } r_o \gg R_C \Rightarrow i_o \approx i_c$$

$$u_o \approx -i_c \cdot R_C$$

$$u_o = -\beta i_b \cdot R_C \Rightarrow u_o = -\beta \cdot \frac{u_{be}}{\beta r_e} \cdot R_C$$

$$u_{be} = u_i \Rightarrow A_u = \frac{u_o}{u_i} = -\frac{R_C}{r_e}$$

$$u_o = -u_i \cdot \frac{R_C}{r_e}$$

$$Z_o = R_C // r_o \approx R_C$$

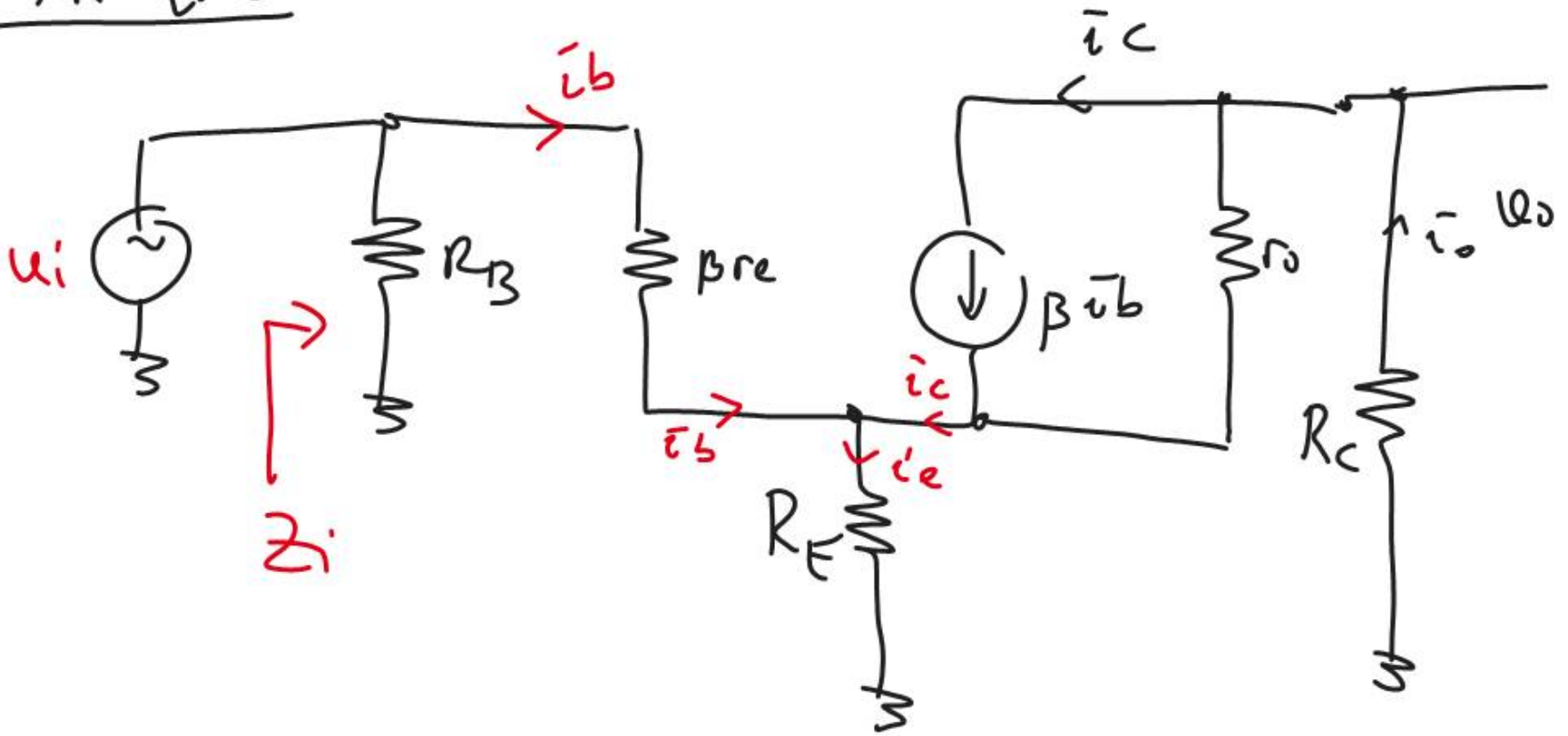
$$A_u = -\frac{6.8 \times 10^3}{21}$$

$$A_u \approx -300$$

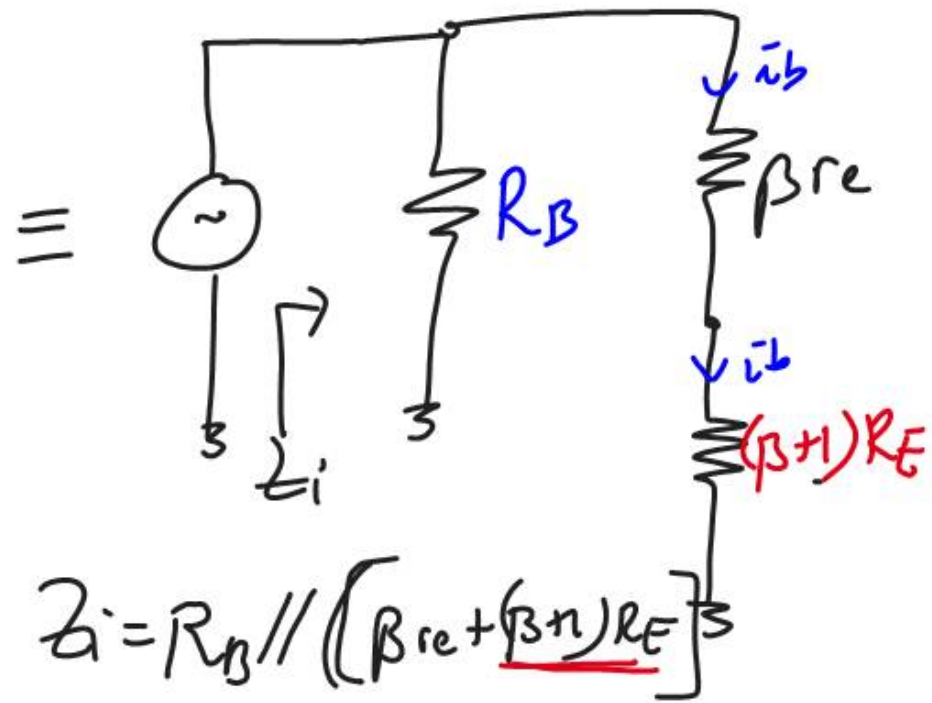
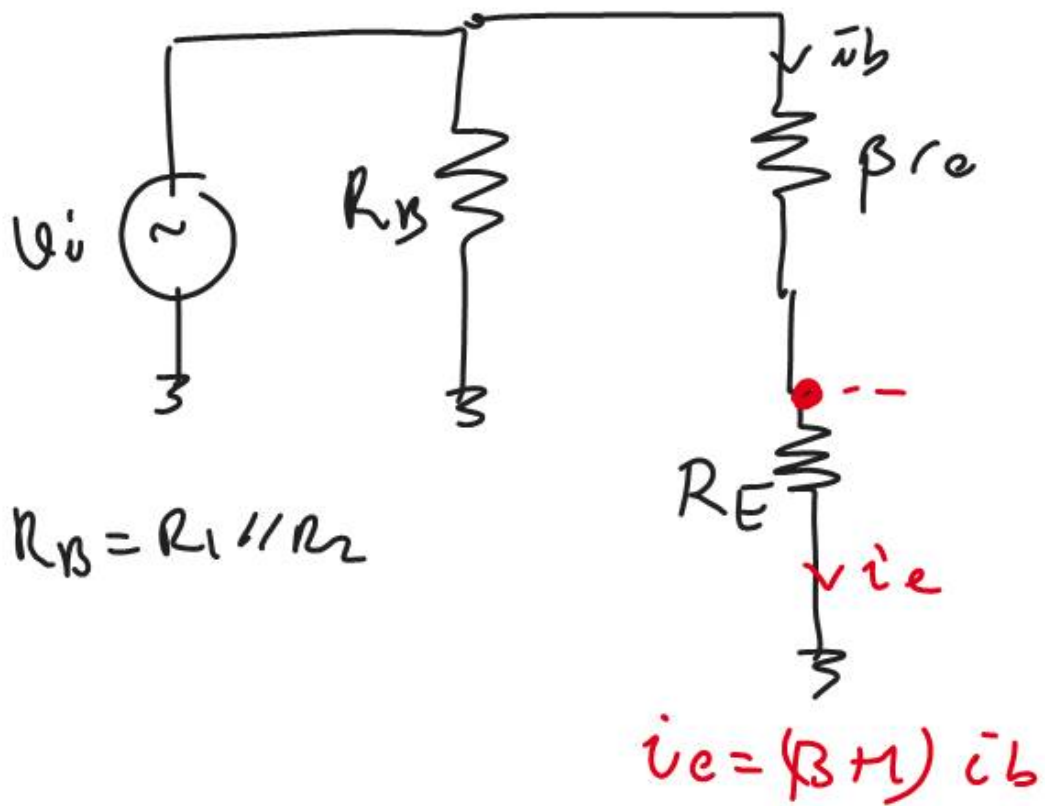
ex If there were no CE:

DC analysis is the same. $\Rightarrow r_e = 21 \Omega$

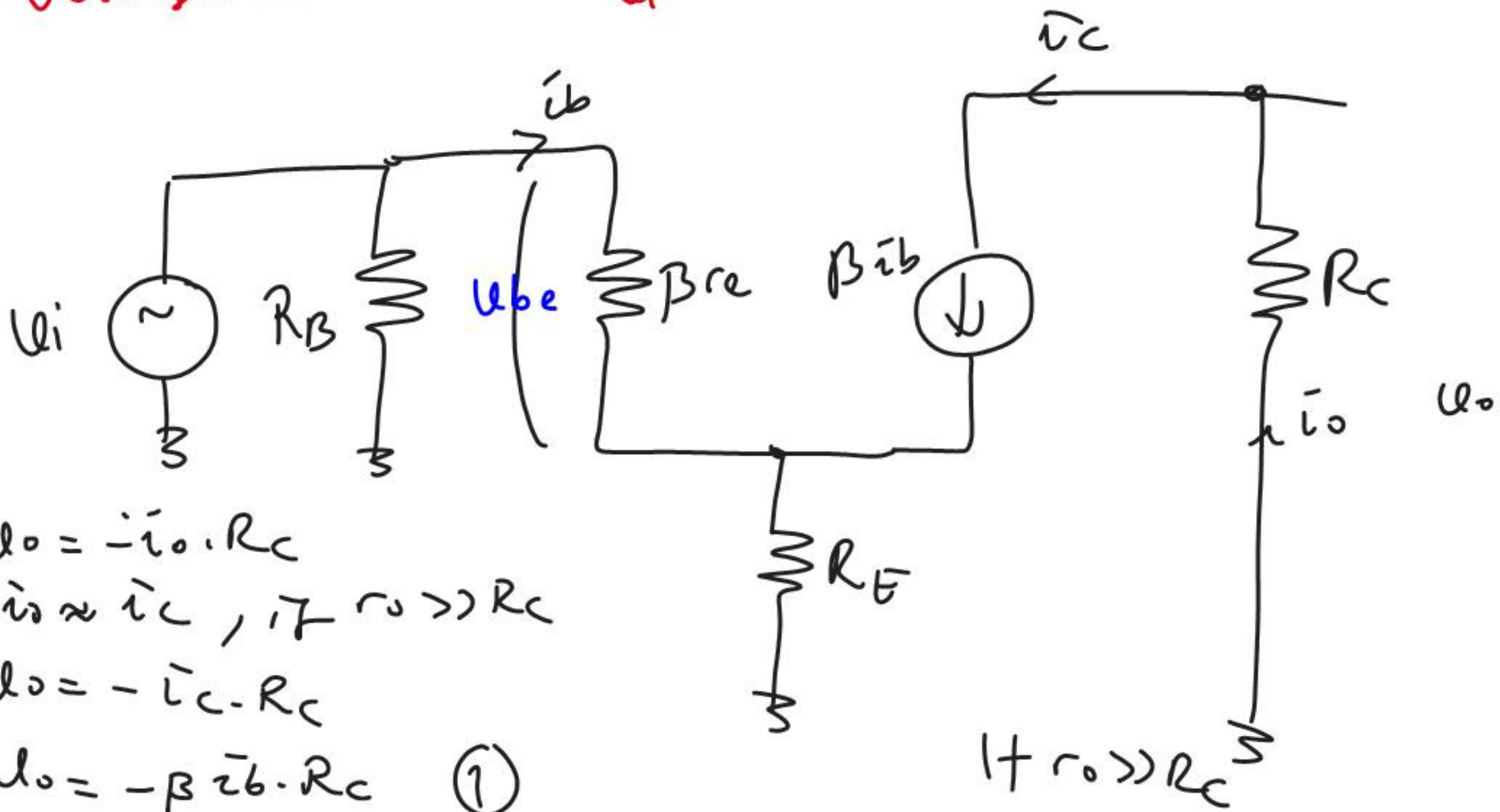
AC Analysis



Input circuit:



Voltage Gain = $A_v = \frac{v_o}{v_i}$



$v_o = -i_o \cdot R_C$
 $i_o \approx i_c, \text{ if } r_o \gg R_C$

$v_o = -i_c \cdot R_C$

$v_o = -\beta \bar{i}_b \cdot R_C \quad (1)$

$v_i = v_{be} + i_e \cdot R_E$

$\beta + 1 \approx \beta$

$v_i = \bar{i}_b \cdot \beta \cdot r_e + \bar{i}_b (\beta + 1) \cdot R_E$

$v_i = \bar{i}_b [\beta r_e + (\beta + 1) R_E] \approx \beta \cdot \bar{i}_b (r_e + R_E)$

$\Rightarrow \bar{i}_b \approx \frac{v_i}{\beta (r_e + R_E)} \quad (2)$

If we insert (2) into (1):

$$V_o = -\beta \bar{i}_b \cdot R_c$$

$$V_o \approx -\cancel{\beta} \cdot \frac{V_i \cdot R_c}{\cancel{\beta}(r_e + R_E)}$$

$$A_v = \frac{V_o}{V_i} \approx -\frac{R_c}{r_e + R_E}$$

$$A_v = -\frac{6.8 \times 10^3}{21 + 1.5 \times 10^3}$$

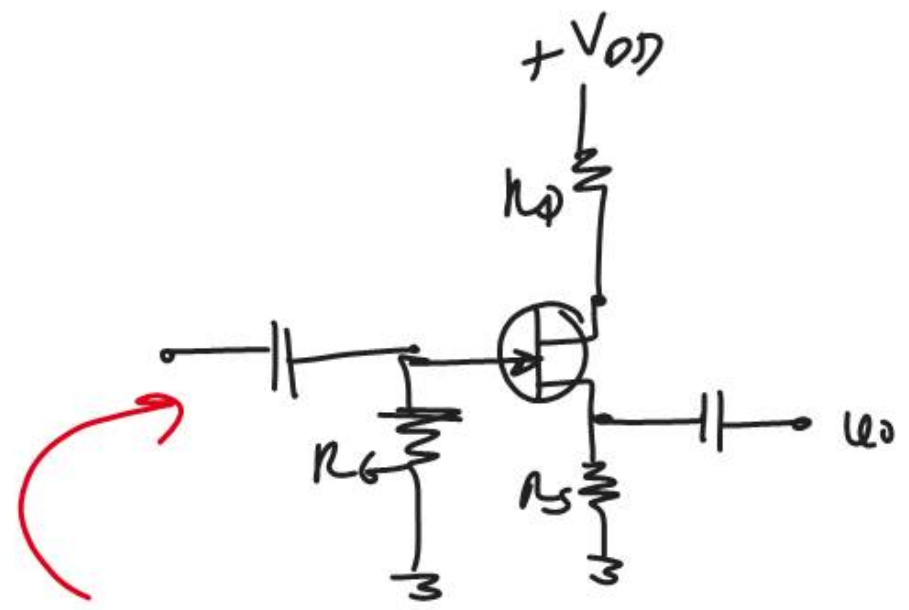
$$A_v \approx -4$$

\therefore with $C_E \Rightarrow A_v \approx -300$

without $C_E \Rightarrow A_v \approx -4$

An unbypassed R_E will reduce the voltage gain too much, although it provides some benefit for Z_i .

EMITTER FOLLOWER



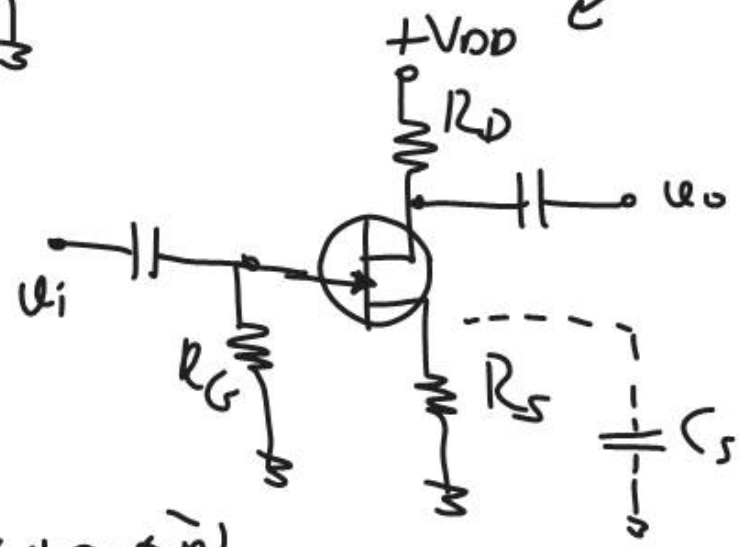
$$A_v = \frac{g_m R_E}{1 + g_m R_E}$$

$$A_v = - \frac{g_m R_D}{1 + g_m R_E}$$

without C_S

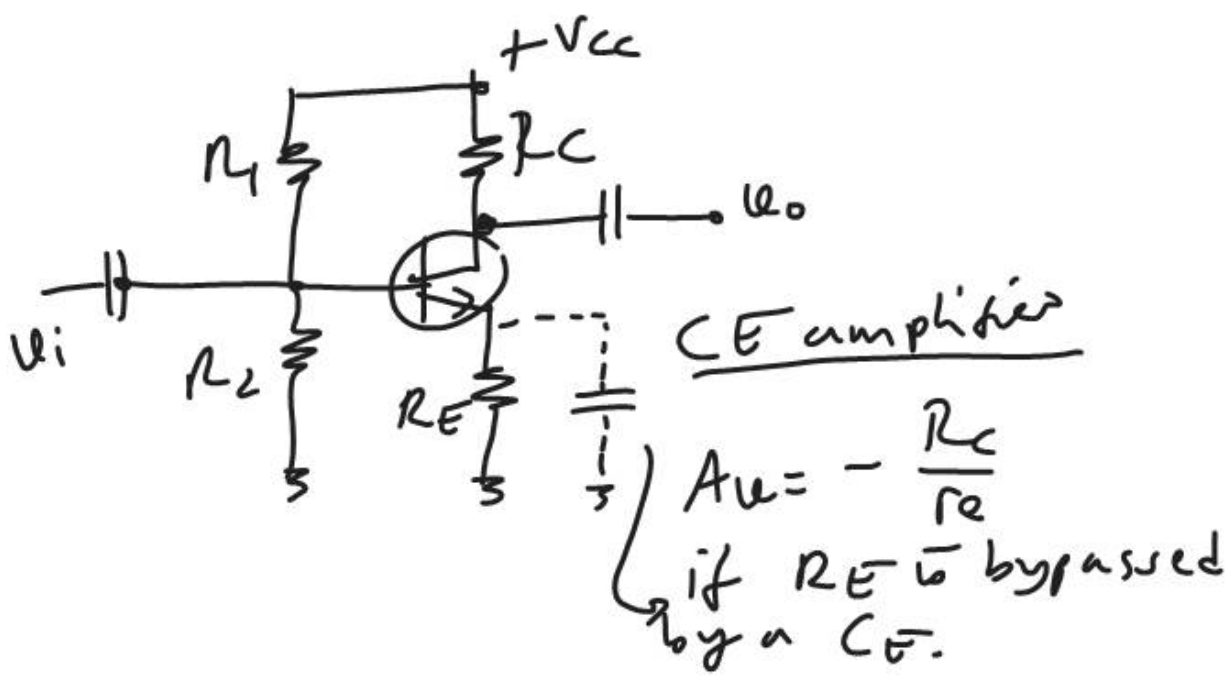
REMEMBER.

The SOURCE FOLLOWER in FETs, (common drain configuration)



$$A_v = -g_m R_D$$

with C_S .

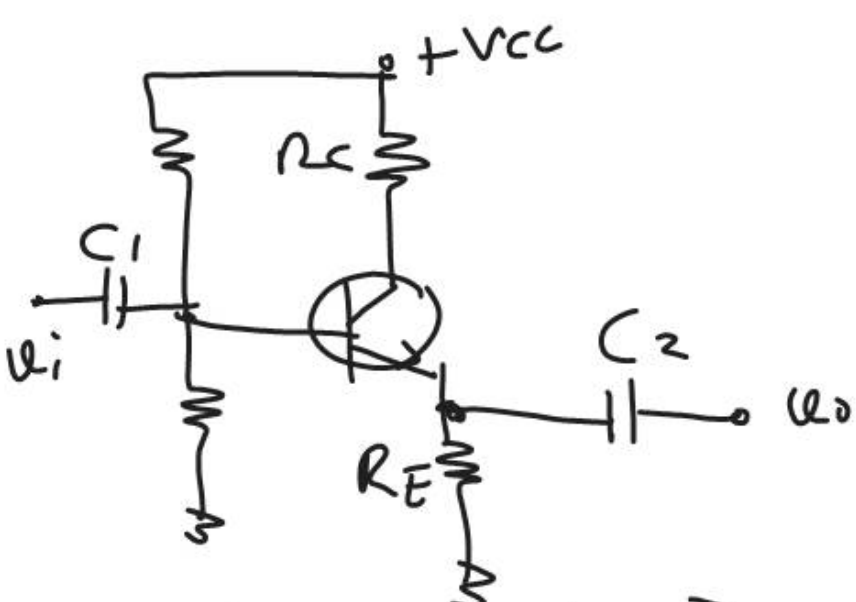


$$A_v = -\frac{R_C}{r_e}$$

if R_E is bypassed by a C_E .

$$A_v = -\frac{R_C}{r_e + R_E}$$

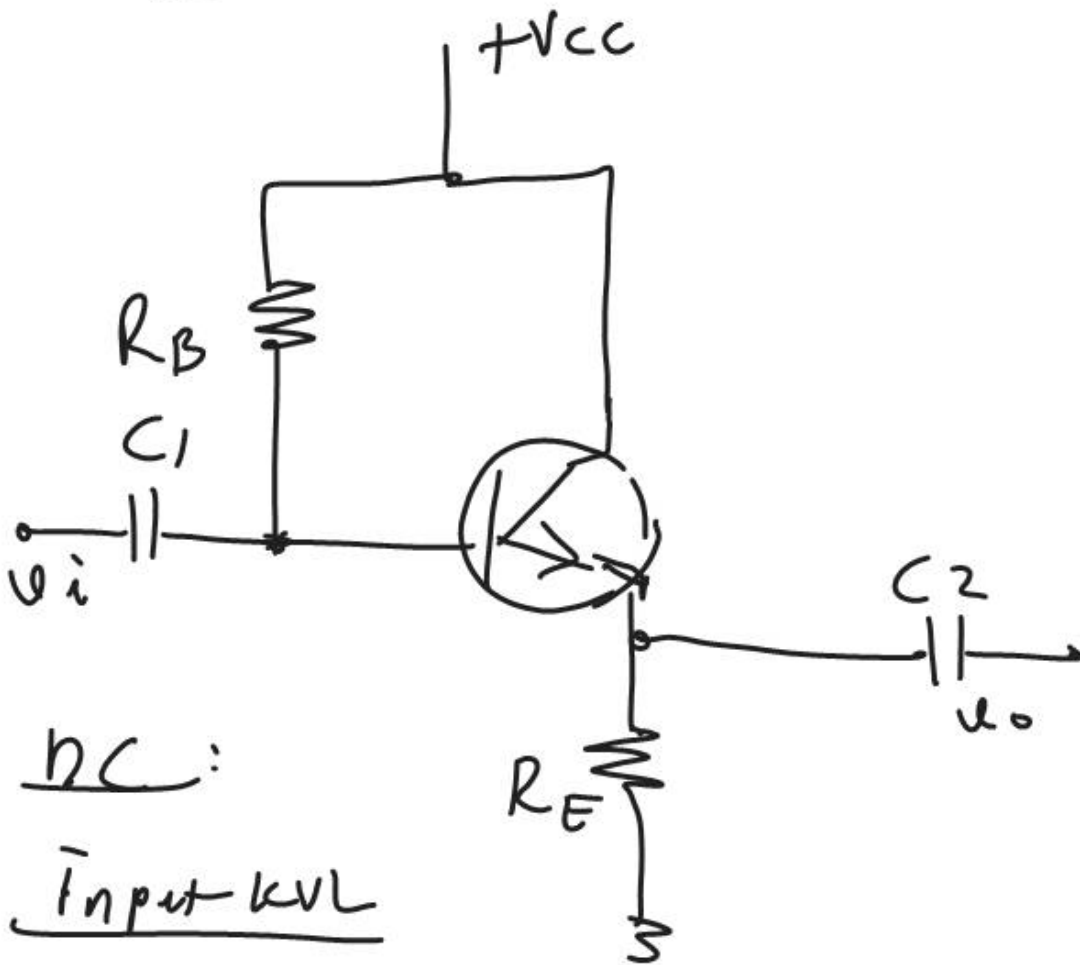
if there were no C_E .



when we are taking output voltage across $R_E \rightarrow$

EMITTER FOLLOWER
(common collector CC)

EMITTER FOLLOWER (Common Collector)

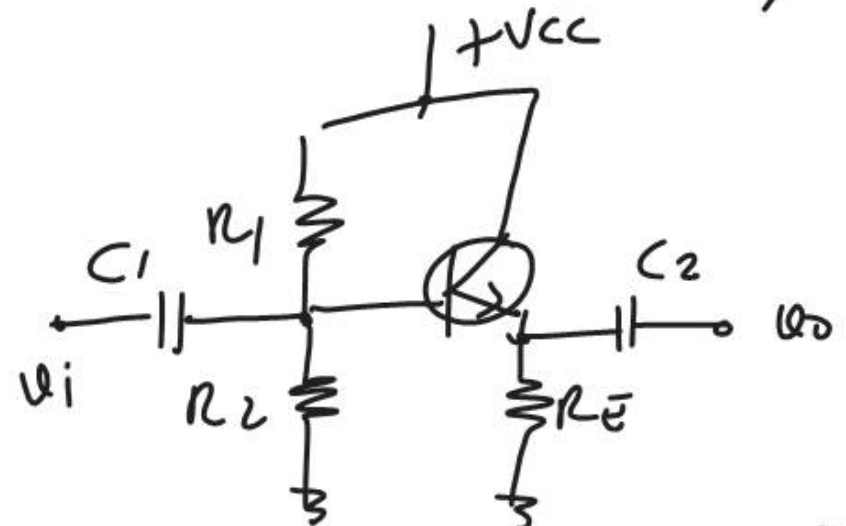


DC:
Input KVL

$$V_{CC} - I_B R_B - V_{BE} - I_E R_E = 0$$

$$I_B = \frac{V_{CC} - V_{BE}}{R_B + (\beta + 1) R_E} \Rightarrow I_E = (\beta + 1) I_B$$

$$r_e = \frac{V_T}{I_E}$$



DC (Voltage Divider)

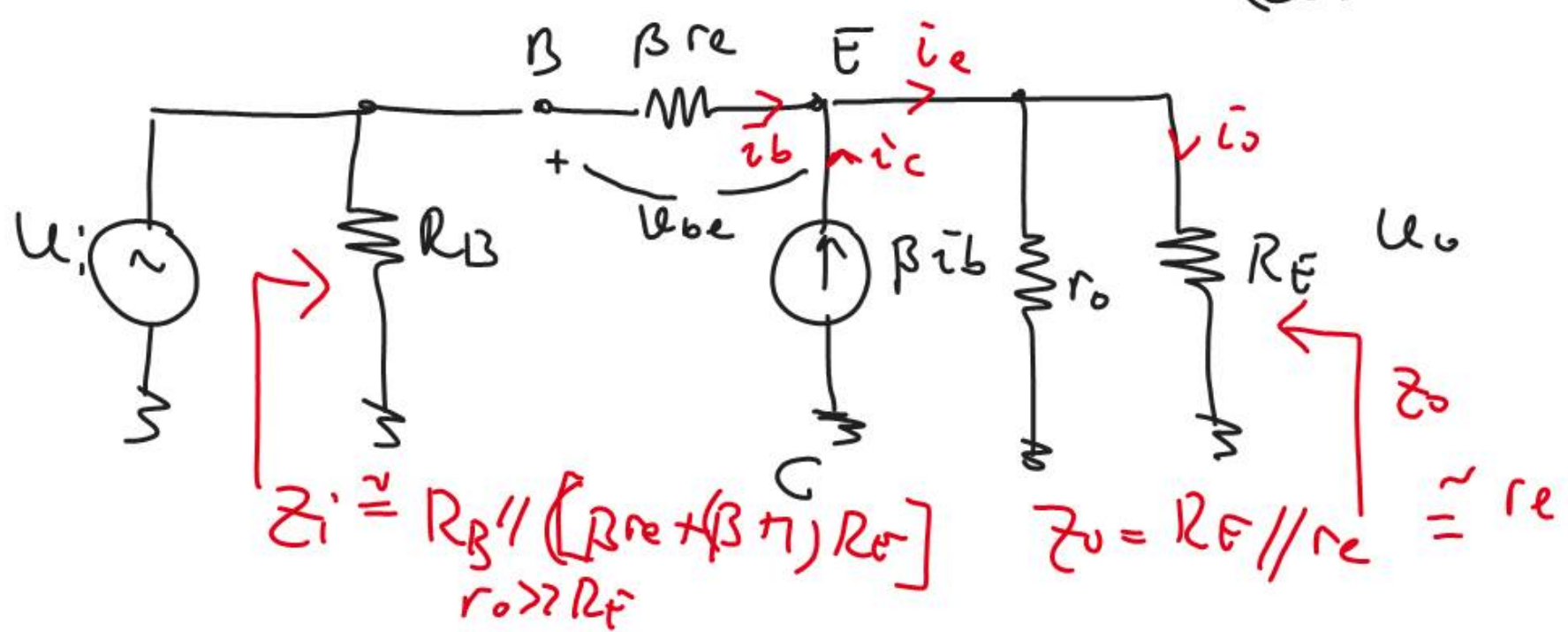
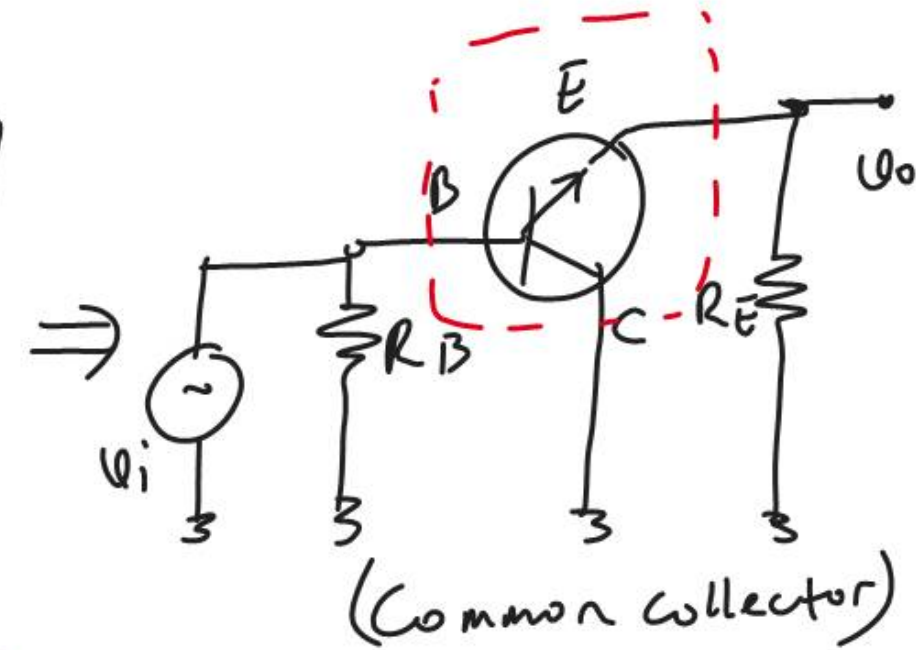
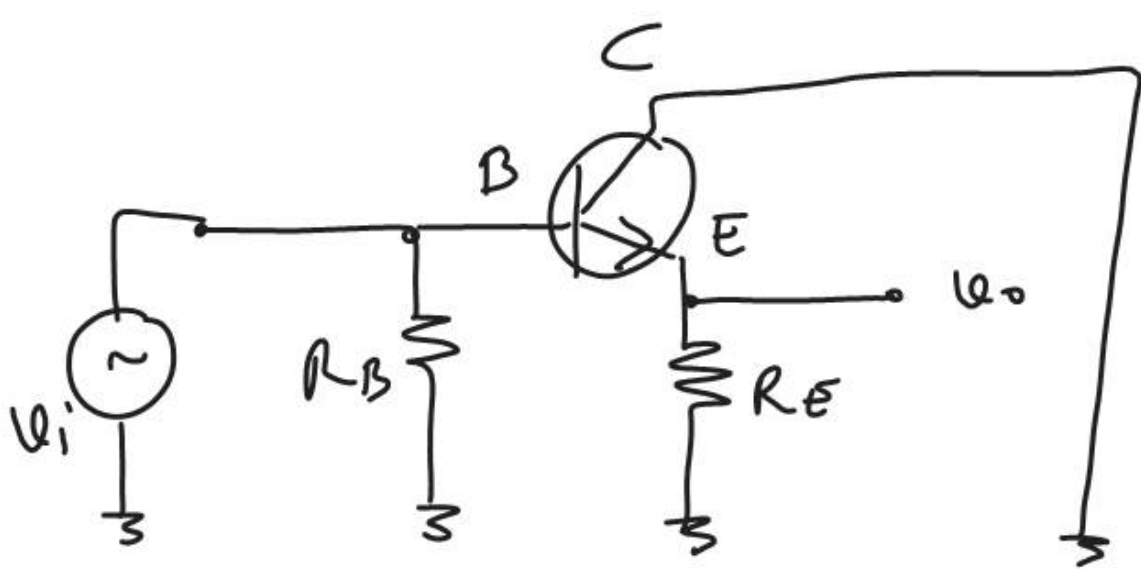
$$V_B = \frac{V_{CC} \cdot R_2}{R_1 + R_2}$$

$$V_E = V_B - 0.7V$$

$$I_E = \frac{V_E}{R_E}$$

$$r_e = \frac{V_T}{I_E}$$

ac analysis



$$v_i = v_{be} + v_o$$

$$v_o = + i_e \cdot R_E$$

$$v_o \approx \frac{v_i}{r_e + R_E} \cdot R_E$$

$$\frac{v_o}{v_i} \approx \frac{R_E}{r_e + R_E}$$

$$A_v \approx \frac{R_E}{r_e + R_E} < 1$$

No phase shift

$$v_i = i_b \beta \cdot r_e + (\beta + 1) i_b \cdot R_E$$

$$i_b = \frac{v_i}{\beta r_e + (\beta + 1) R_E}$$

$$i_e = (\beta + 1) i_b$$

$$i_e = \frac{(\beta + 1) v_i}{\beta r_e + (\beta + 1) R_E}$$

$$i_e \approx \frac{v_i}{r_e + R_E}$$